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Title: Development and operation of Pulse Magnet at LANL's PFF

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Development and operation of Pulse Magnet at LANL's PFF

Doan N. Nguyen





OUTLINE

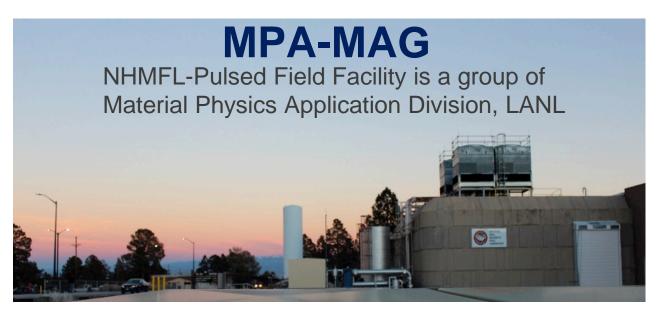
- 1. Overview of Pulsed Field Facility at LANL
- 2. Performance and design improvement of 65 T workhorse magnets
- 3. Performance, failure and rewinding progress of 60 LP
- 4. Performance and challenge of 100T
- 5. Introduction of future 80 Duplex magnet
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OVERVIEW OF NHMFL's PFF at LANL





Our mission is to provide:

Extreme magnetic fields at the Pulsed-Field Facility in support of the National High Magnetic Field Laboratory's User Program



NHMFL User Program



Magnet Engineering



High-Field Science

http://nhmfl.lanl.gov

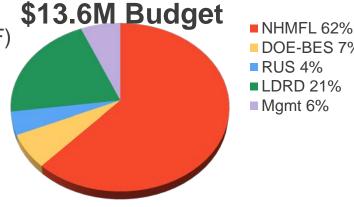
MPA-MAG Primary Projects

Strategic Partnership Projects

- NHMFL-Pulsed Field Facility User Program (FSU/NSF)
 - (~\$8.4M/yr x 5)
- **DOE Basic Energy Sciences**
 - Science of 100 Tesla
 - (Harrison \$0.9M/yr x 3)







DOE-BES 7% ■ RUS 4% ■ LDRD 21% ■ Mgmt 6%

Weapons & Global Security Programs

- Science Campaign 1 & 2: Aging & EOS via RUS Resonant Ultrasound Spectroscopy
 - (Maiorov Co-I **\$0.396M**)



LDRD - Directed Research

- Defect Induced Emergent Magnetism
 - (Crooker ER 2015 **\$0.34M x 3**)
- Fluctuating Domains in Antiferromagnets for Sensing and Switching Applications
 - (Zapf ER 2017 **\$0.35M x 3**)
- Electronic Structure of putative topological Kondo insulators
 - (Chan ER 2018 **\$0.32M x 3**)
- Scalable dielectric technology for VLF antennas
 - (Singleton ER 2018 **\$0.296 x2)**)
- Uncovering the role of 5f-electronmagnetism in the electronic structure and equation of state of plutonium (U)
 - (Harrison DR 2018 **\$1.52M x 3**)



John Singletor

What is Unique @ the NHMFL

1.43 Billion Watt Generator

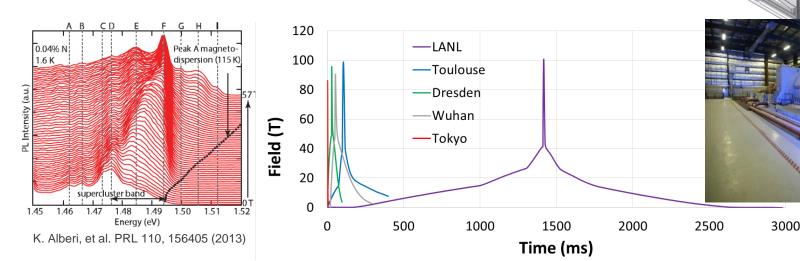
 Capable of delivering 600 Mega-Joules of electrical energy in a safe and reliable manner many times each day

100 tesla non-destructive magnetic fields

 More than 10000 times longer duration pulse = unprecedented scientific resolution

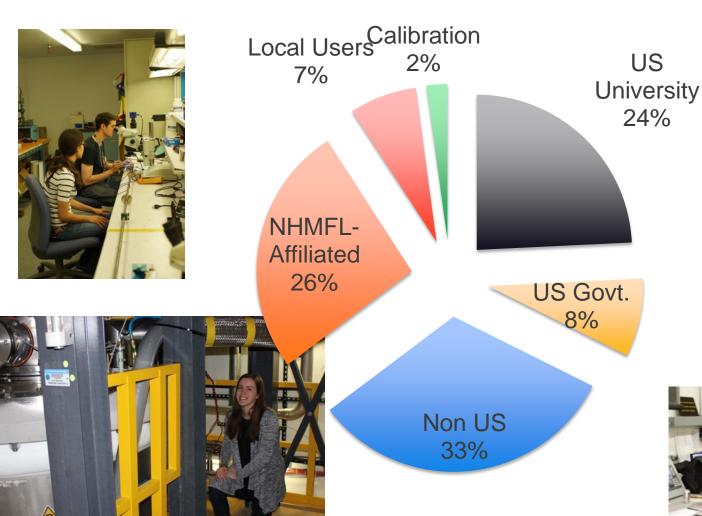
60 tesla controlled waveform magnet

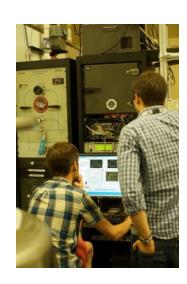
- Heat capacity (relaxation method)
- High resolution photo-luminescence
 - True optical spectroscopy (1000s of spectra)



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Where do NHMFL-PFF Users come from?







The Pulsed Field Facility



60,000 ft²
16 Magnet stations
10 Pulsed
6 SC

13 Scientists/Eng

9 Technicians

6 PDs

13 students

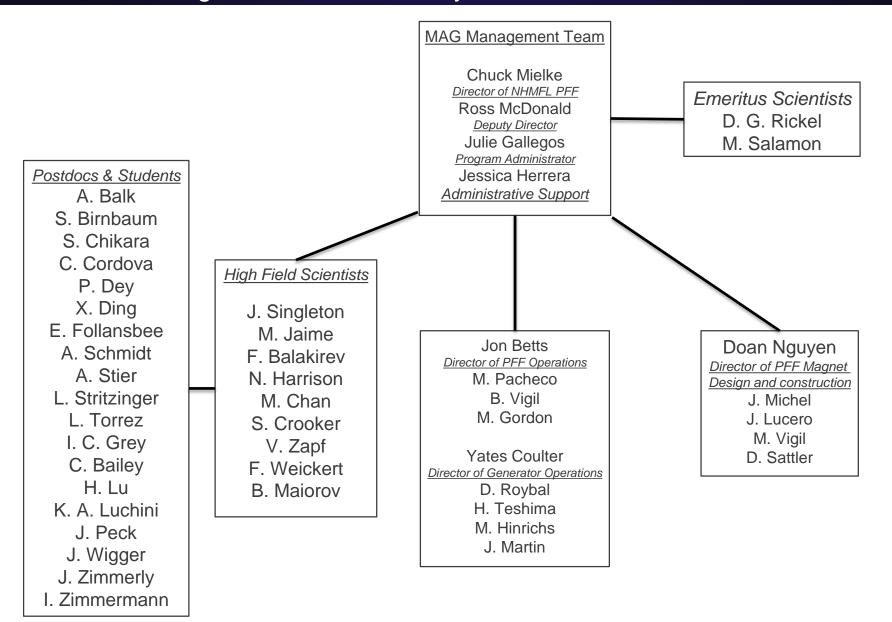
3 Admin

2 Eng Contract

46 Total People

200 users/yr

MPA-MAG Organizational Chart July 2017



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Strategically investment in Helium recovery

- Helium liquefaction Investment avert major issue with helium access for users
- Recovery rate ~90%

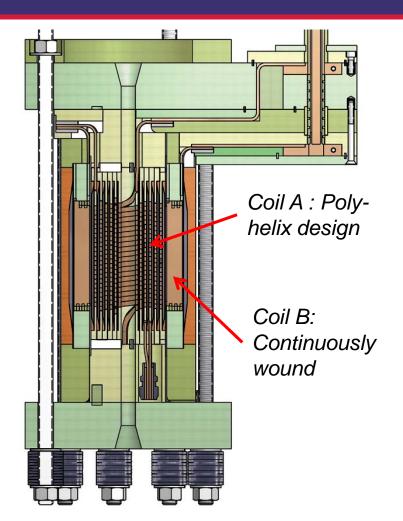
- FSU major Equipment
- LANL G&A funds paid for NHMFL Labor, safety engineering and utility installation costs



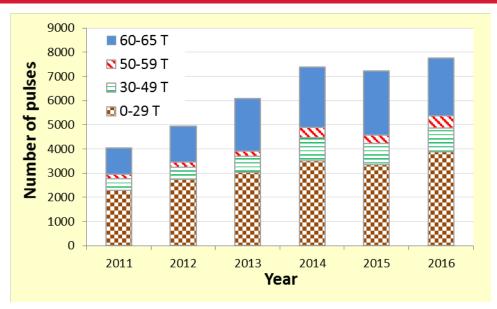
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65 T workhorse magnet operation



Overview of 65 T magnet cross-section



- 4 cells of 65 T magnets
- More than 7000 shots in last three years
- ~2500 shots above 60 T
- 4 6 magnets failed each year



65 T Workhorse Magnet – Redesigned reinforcement of coil A

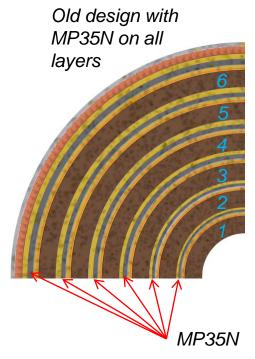
Installing wraps of MP35N thin strip is challenging and time consuming:

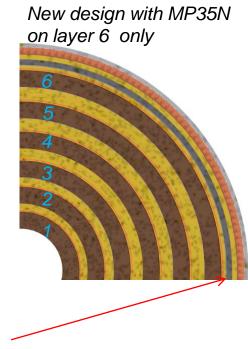
 difficult to pack MP35N strip tightly due to its ripple and non-uniform thickness



Replacing MP35N by Zylon fiber and S2-glass tape composite helps:

- Reduce the manufacturing time significantly, improve the quality control
- Mechanically stronger
- Reduce the material cost (MP35N strip is expensive)



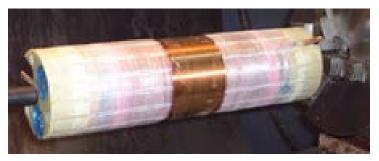




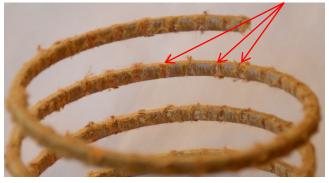
65 T Workhorse Magnet – New cooling technique

Without cooling channels, magnets take 2.5 hours for cooling



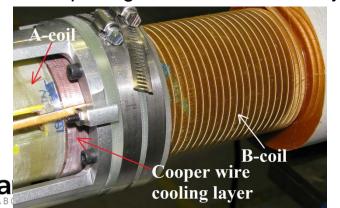


Cooling channels on coil A for LN to flow between coils A and B: Cooling time down to 25 – 30 minutes

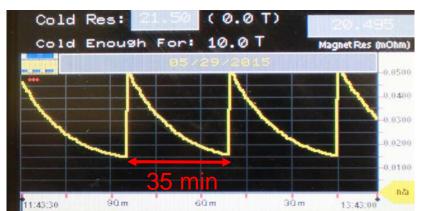


Issue: Conductor of coil B collapsed into cooling channels due to post-pulse compression, causing instability and wire insulation damage

New cooling technique: layer of insulated, 16 gauged copper wires laid along coil A. No eddy current issue, no mechanical impact, good thermal efficiency







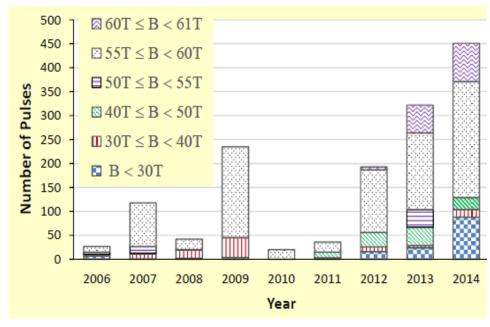
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60 T Controlled Waveform Magnet



- Consists of 9 nested coils, powered by 1.4 GW generator
- 60-T peak field in 32 mm bore
- 2500-ms pulse length with 100-ms flattop
- Controllable waveforms to meet some special requirements from user



- First assembly failed in 2000
- Rebuilt magnet started operating in 2006
- Soft failure at mid-plane of coil 7 in December 2014.
- Totally, delivered 1453 shots, 144 shots with 60 ≤ B ≤ 61T and 888 shots with 55 ≤ B ≤ 60 T



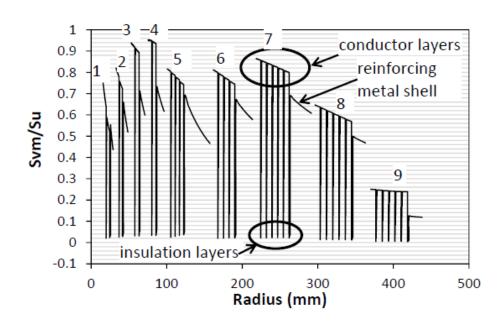
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Slide 16

Mechanical Performance of 60 T Controlled Waveform Magnet

- von Mises stresses in coils 3, 4 and 7 are the highest
- Svm/Su ~0.95 for conductors in coils 3 and 4
- Stress in conductor of coil 7 also reaches ~0.87 of the ultimate stress
- These results explain for considerable dilation of mid-plane of coil 3,4 and 7, observed from autopsy after magnet's failure. Other coils are ok!

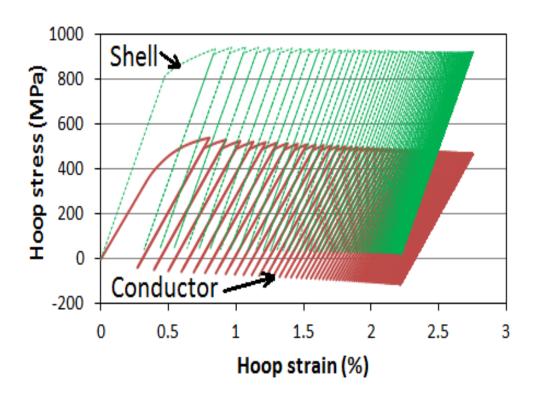
Mid-plane von Mises stress normalized to the ultimate stress (Svm/Su) for all 9 coils for a typical 60 T shot





Understanding the dilation in 60 T CW magnet by preliminary cyclic simulation

- Magnet delivered 195 shots with 59≤ B
 ≤ 61 T
- Using data from fatigue tests of conductors/reinforcing material, preliminary cyclic simulations for 195 shots of 60 T have been done
- In no-load condition after each pulses, conductor is compressed due to plastic elongation while the shells is stressed as expected.



Stress-strain relation in hoop direction for the conductor and reinforcement shell of coil 4 (the weakest coil) after 195 shots at 60 T

Slide 18



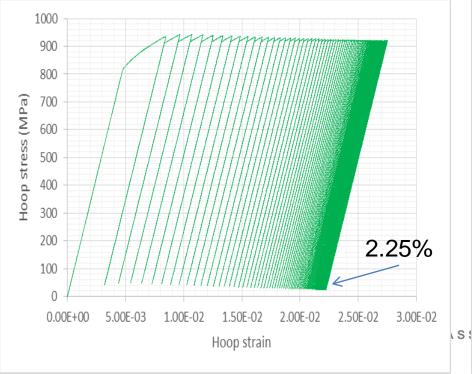
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Cyclic calculation for 60T CW magnet

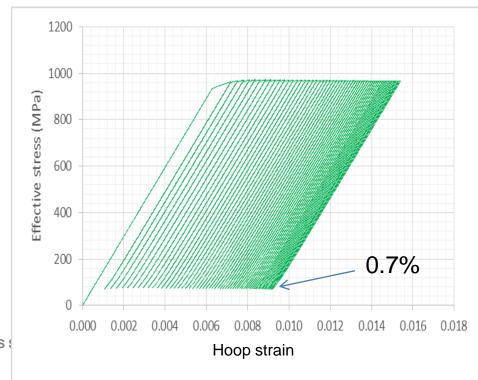
Performed for 195 cycles of full field:

- Residue hoop strain of Ni40 metal shell of coil 4 is 2.25 %
- Residue hoop strain of Ni40 metal shell of coil 7 is 0.7 %
- The computational results are close to the reality (within 20%)

Hoop strain in metal reinforcement of coil 4



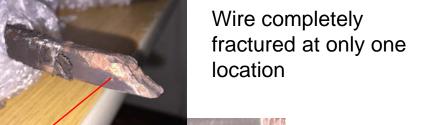
Hoop strain in metal reinforcement of coil 7



Autopsy of the failure of coil 7 – 60T LP magnet



Happen in several turns near the mid-plane



Wire shorten and deformed due to heating and asymmetric compression



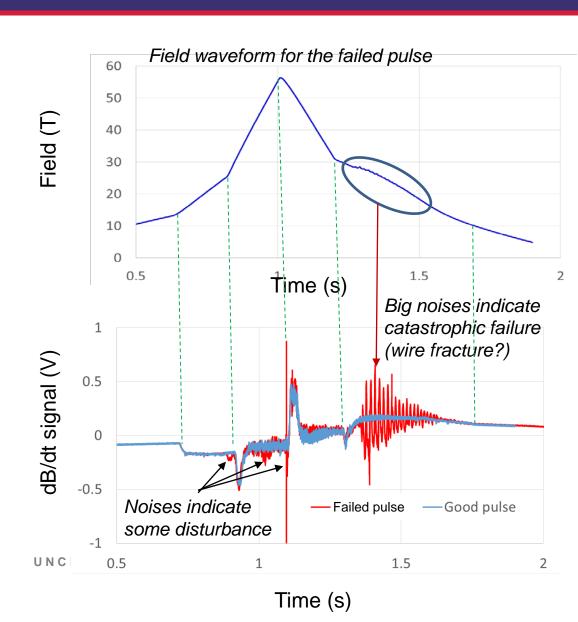
Arcing turn-to-turn all around the coil



Slide 20

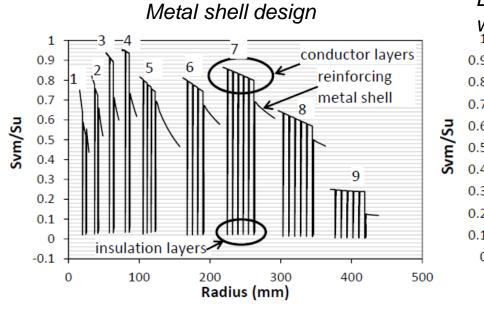
Autopsy of the failure of coil 7 – 60T LP magnet

- Driven by three power supplies
- dB/dt signal for the failed pulse shows some low noises in the first half of the pulse (arcing starts and propagates?)
- Larger noise happens in the second half of the pulse indicate a catastrophic failure (wire fracture?)
- The insulation breakdown initiated the failure
- That prediction is also reasonable because both calculation reality show considerably higher stresses in coils 3 &4 which are still survive
- Wire insulation need improvement and better quality control

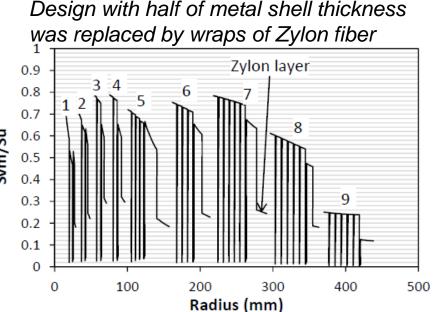


Proposed plan to improve mechanical performance for 60 T CW magnet

- Magnet is a very important, versatile tool for our users => will be rebuilt asap
- Partially replacing the metal reinforcing shell with wraps of Zylon fibers, especially for coils 3, 4 and 7, can improve the mechanical performance



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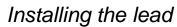
- More analyses will be carried out for better optimization
- The proposed approach using Zylon fiber does not require significant structural modifications and would not affect the manufacturing time

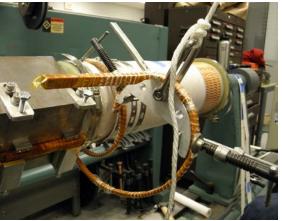
Production of 60T LP magnets at NHMFL-FSU campus

- Need to rebuild coils 3, 4 and 7 for 60 T LP magnet
- Developed winding capability at NHMFL-FSU to wind big pulsed magnet coils: better quality control, more R&D work
- Production of a model coil was finished, production of 3 and 4 will be started soon

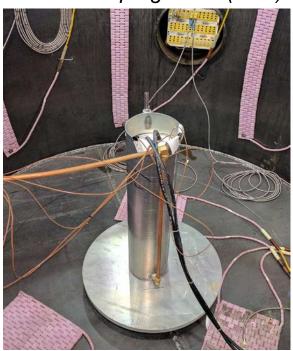


Winding the coil





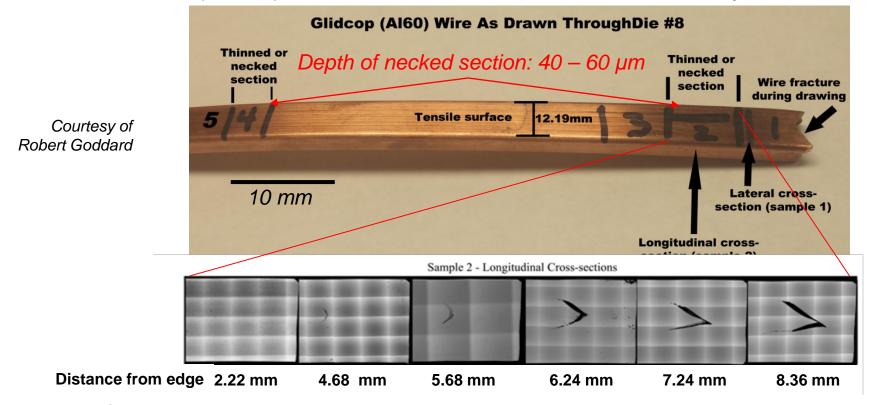
In chamber, ready for Vacuum Pressure Impregnation (V.P.I)



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Chevron breakage during drawing of wire for coil 7

- Glidcop AL60 wire for coil 7 needs 10 drawing passes (dies) to meet mechanical strength
- Wire was fractured at pass #8
- Wire has thinned (necked) sections which are difficult to detect with bare eyes



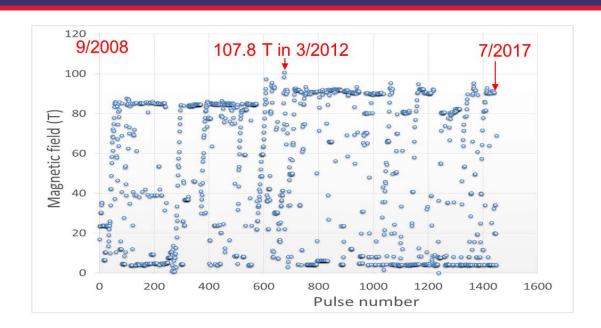
- Detect Chervon cracks inside wire at thinned section
- Investigation to improve drawing process (change die schedule, die angle, drawing speed, lubricants) is underway to produce good wire for coil 7
- May need to inspect the wire for internal crack before winding (Xray, ultrasonics)

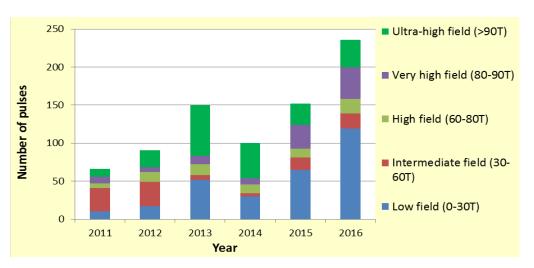
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100 T multi-shot magnet performance

- Total ~ 1500 shots
- 230 shots above 90 T
- 560 shots above 80 T
- 3.5 hours cooling time between full field shots
- Faster cooling design (2 hours) is desired and being developed





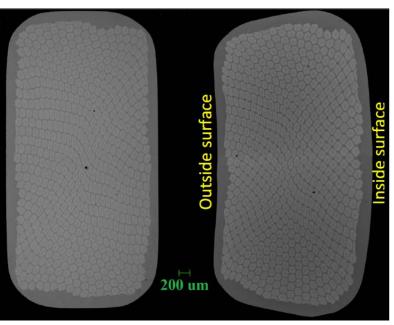
100 T Multi-shot Magnet - Conductor Issue

- Use Cu-Nb nano-composite wire (UTS ~1.2 GPa at 297K)
- Mechanical properties not very consistent over long length or between purchases
- Wire sometimes get fractured when wound on 10-mm
 OD mandrel for 100-T magnet
- Effect of small radius bending on conductor deformation/strength must be investigated
- The wire experienced a considerable deformation as wound into 10 mm bore helix
- Areas of Nb filaments increase by ~ 16 %
 near the inside surface and decrease by 19 %
 near outside surface.
- Wire compressed 6% inside and stressed 19% outside
- For more details see presentation 4OrBB_03

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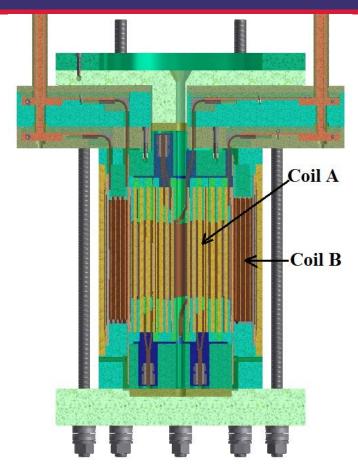




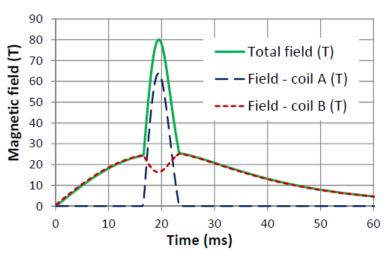
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Prototype 80 T Duplex Magnet



Overview of 80-T duplex magnet (15 mm bore, coils A and B independently driven by 2 cap-banks)



Field profile for a 80 T

- For the 80 T shot, the maximum Svm/Su = 0.8 for conductor and = 0.58 for reinforcement materials
- Should have lifetime for 1000 shots of 75 T for regular operation
- Scheduled to be tested in Jan 2018



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Construction of 80 T duplex magnet and user duplex cell were completed



1st duplex magnet



User duplex cell with housing for magnet under the platform

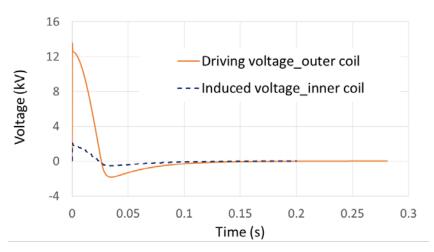
- 4 MJ capbank will be shared between duplex magnet and four 65 T magnets
- Capbank was modified and reconfigured so that the test and operation of duplex do not impact much on operation of our workhorse 65 T magnet
- Construction of duplex cell with user platform was completed



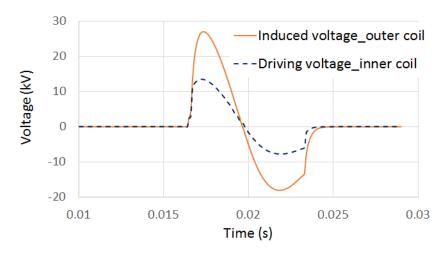
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MOV protection bank was designed and now under construction

What happen if "misfired" situation occurs with a 80 T shot?

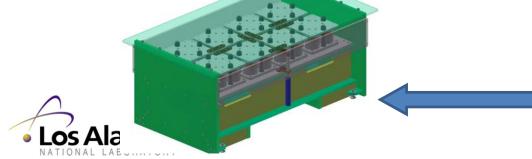


 Outer coil is energized with 14 kV generated induced voltage of ~2 kV on the inner coil if it is in open circuit



- Inner coil is energized with 13.5 kV generated induced voltage of ~27.2 kV on the outer coil if this coil is open
- Thin MP35N layers with their low electrical conductivity do not help much in decoupling between the coils

Need a metal oxide varistor bank connected in parallel to the outer coil to protect its capbank and control electronics



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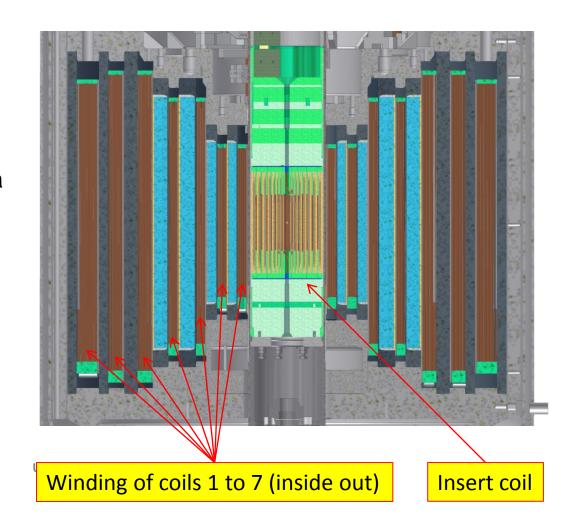
Propose to upgrade the present 100 T magnet in the new funding cycle (2018 -2023)

Proposal was submitted fall 2016, should receive final decision of NSF this fall:

Upgrade the present 100 T magnet to the range of 115 -120 T

Field contribution (100.8T):

- Outsert's coil groups driven by 3 power supplies powered by a 1.4GW generator
- Outsert: 40.6T (2500 ms)
- Insert : 60.1T (15 ms, c-bank)
- Maximum magnetic energy at 100 T: 153 MJ
- Ohmic loss: 90 MJ



Approach for 115 T using upgraded outsert magnet

Remove C1 and C2 of the outsert magnet to use that space for insert windings with much higher current density



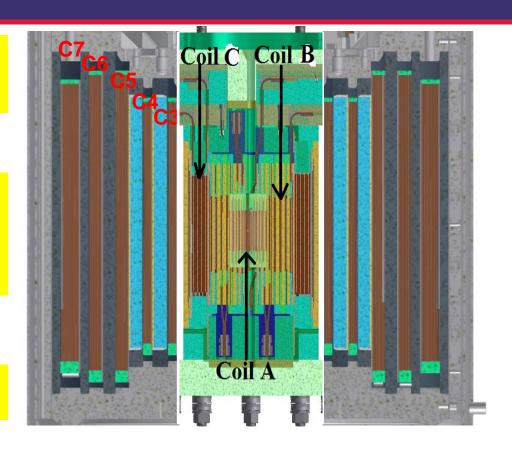
Upgrade/redesign C3 and C4 to provide background field of 30 T in 45 cm bore:

- Use better conductor (CuNb wire)
- Replace SS301 shells by a combination of Ni-40 and Zylon



Use triplex insert powered with new cap-banks:

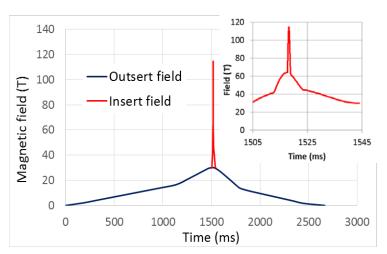
Require new 30 kV, 11 MJ Capbank



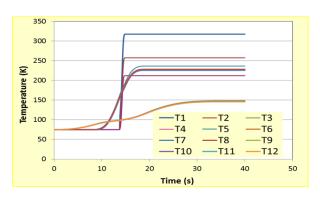
We current have spare coils for C5, C6, C7, it is possible that we can build a new 115 T if funding is available:

- New pit with supporting structure
- New C3 and C4
- New capbank

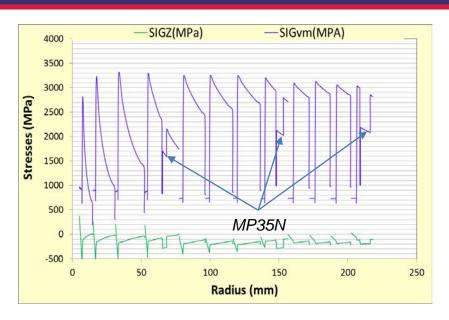
Field profile for 115 T magnet and mechanical/thermal performance of the insert coil



85 T triplex insert in 30 T background field



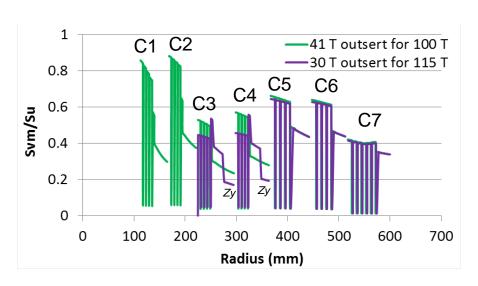
Temperatures in all 12 winding layers during a full field pulse are below 350 K



Stress level of the insertfor a full-field pulse:

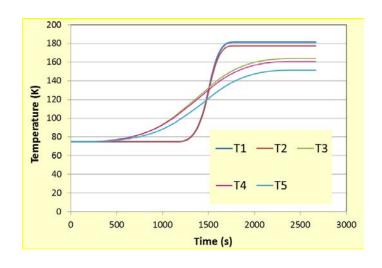
- Peak Von Mises stress in Zylon 3300 MPa
- Peak compression axial stress is 500 MPa
- Higher risk in lower energy coil, expect the inner most coil fails first
- MP35N layer outside each sub-coil to prevent failure to transfer from low energy coil to high energy coil

Mechanical and thermal performance of 115-T outsert compared to present 100 T



Normalized stress Sv/Su in the present 100T outsert and proposed wide-bore outsert for 115T

- Generally stress is nearly on the same level
- With Zylon and new CuNb conductor, coils 3 and 4 of the proposed outsert have lower stress level, possibly deliver higher field



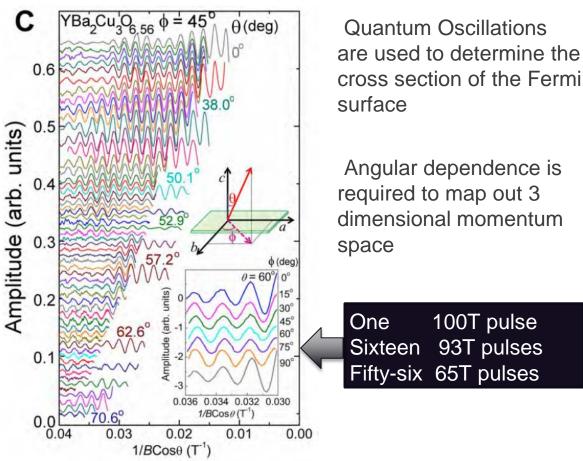
Temperatures in the winding layers of proposed outsert magnet for a full-field pulse are all below 200 K

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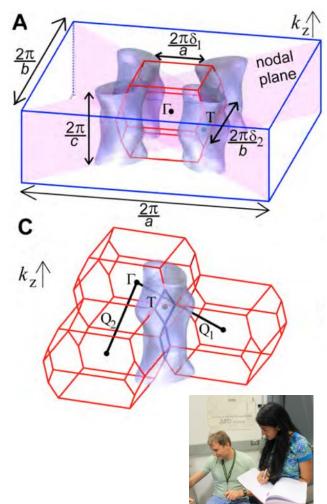
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Exhaustive work requires the best and most reliable technologies



Angular dependence is required to map out 3 dimensional momentum

100T pulse 93T pulses Fifty-six 65T pulses



Electronic excitations in atomically thin semiconductors

- Monolayer transition-metal dichalcogenides belong to a new class of atomically-thin semiconductors that show great promise for advanced optoelectronic applications
- Magneto-transmission spectroscopy in pulsed magnetic fields to 65 teslas revealed—for the first time—how the binding energy and size of the excitons depend on the dielectric constant of the surrounding material. This work shows that optical properties of 2D semiconductors can be tuned by design.

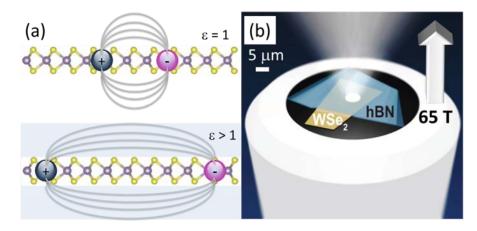


Figure 1: (a) 2D excitons in monolayer WSe₂: As dielectric screening from the surroundings increases, their size grows and binding energy drops. (b) The experiment: monolayer WSe₂ is affixed to an optical fiber and encapsulated.

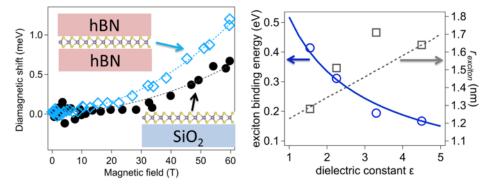


Figure 2: (a) Quadratic diamagnetic shift to 60T gives the exciton radius ($r_{exciton}$). (b) Calculated and measured exciton binding energy and $r_{exciton}$ versus average dielectric constant ϵ of the surrounding environment.



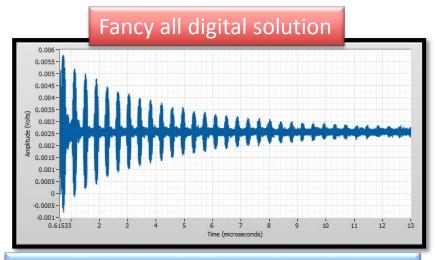
A.V. Stier, N.P. Wilson. J. Clark, X. Xu & S.A. Crooker, "Probing the influence of dielectric environment on excitons in Monolayer WSe₂: Insight from high magnetic fields." *Nano Lett.* **16** (11), 7054-7060 (2016)



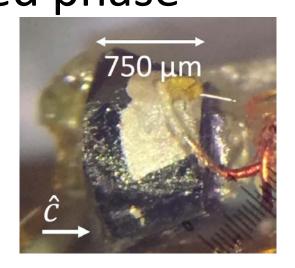
Thermodynamic signature of the field induced phase

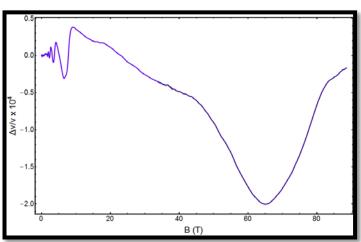
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- pulsed echo ultrasound yields change in sound velocity and attenuation @ 300 MHz
- Y-cut LiNbO3 transducer
- V^{\sim} 5km/s \rightarrow sub mm samples
- 100kHz pulse rep rate.
- Phase measurement of multiple echos gives 1pt in 10⁶
- TaAs single cristal



User: Brad Ramshaw → Cornell



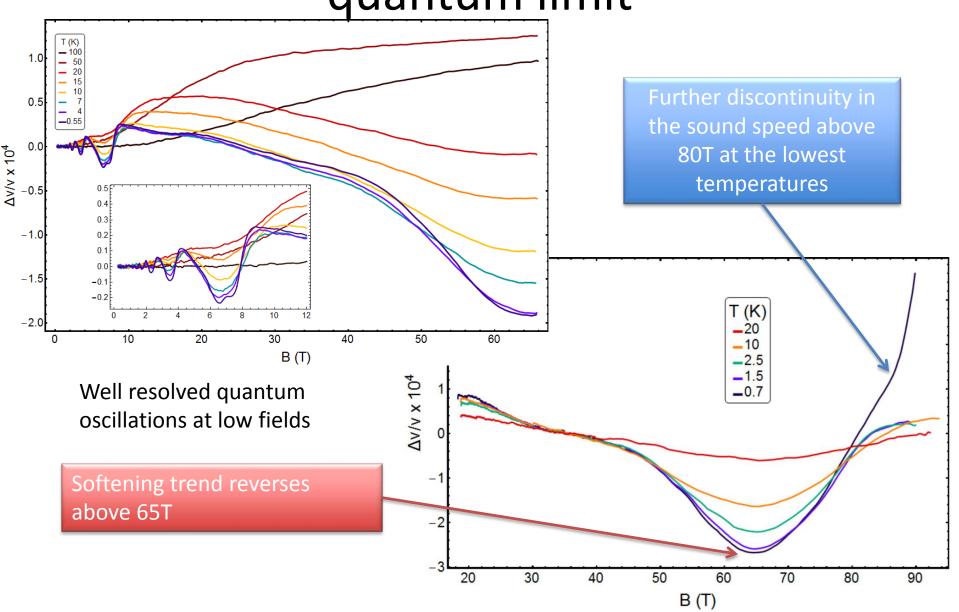


Change in the speed for ~k//B//c, where ~k is the propagation wavevector of the longitudinal sound

M

Sound speed in the quantum limit

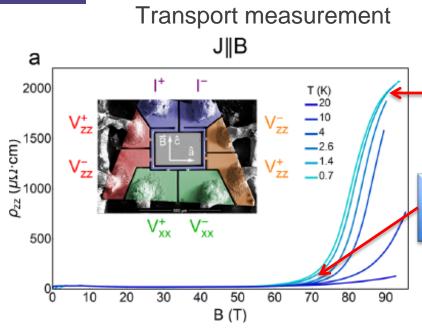




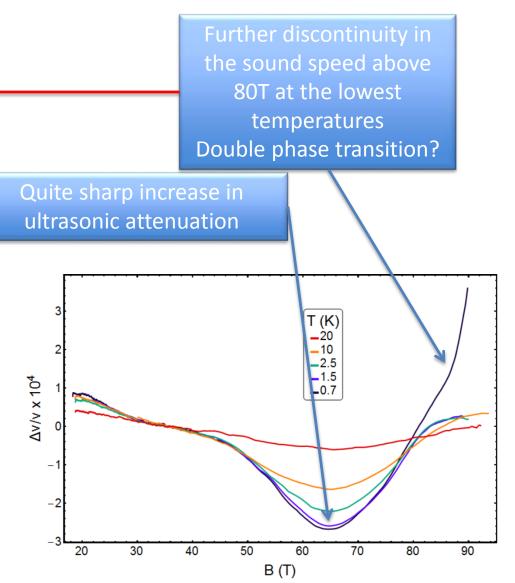


Similar behavior for transport and RUS measurement





Brad Ramshaw: arXiv:1704.06944v1 [condmat.str-el] 23 Apr 2017



Thank You & Question

